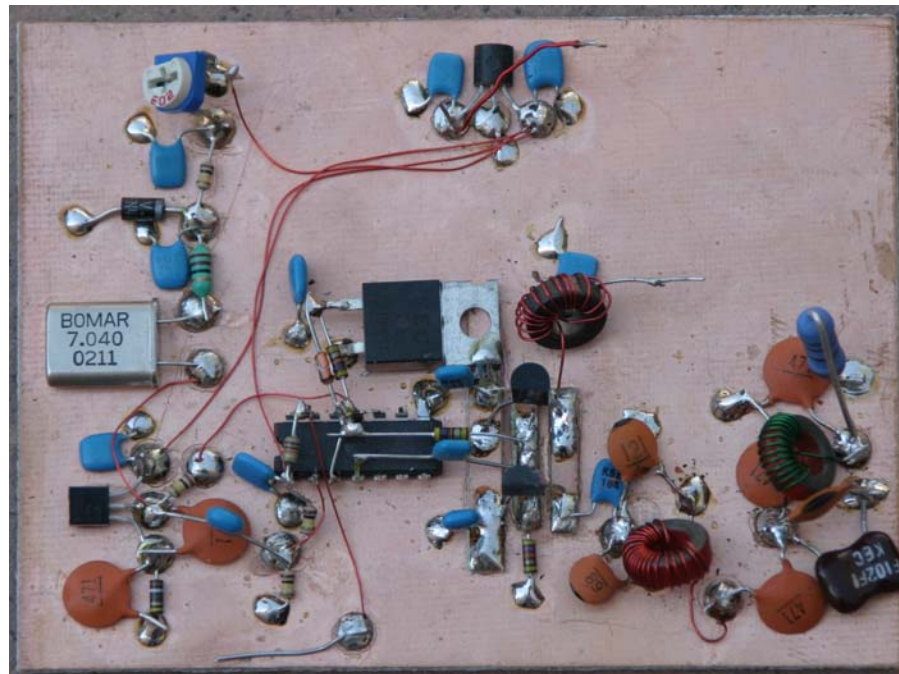


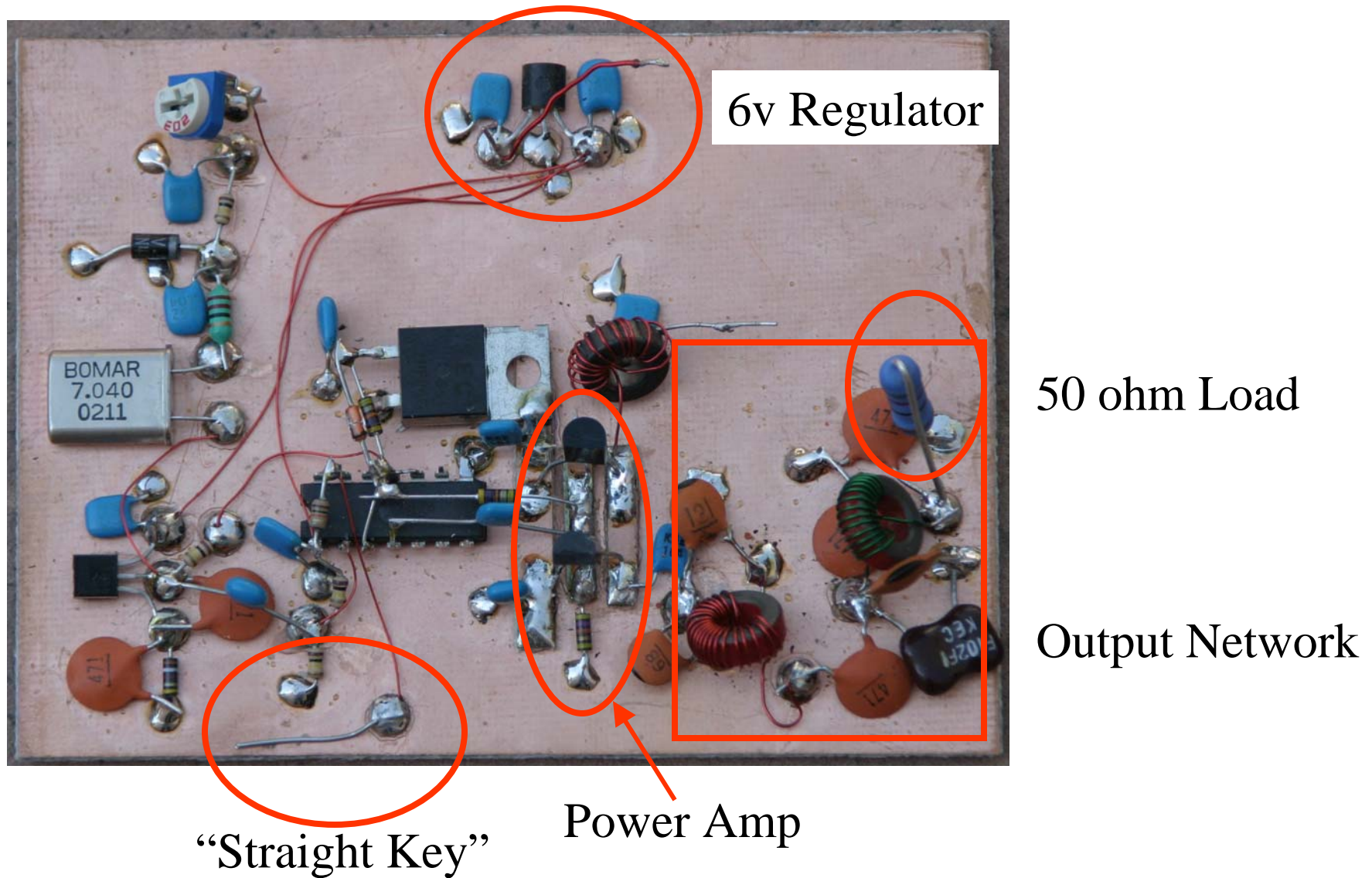
Class E Amplifiers

Part 1: Class E Basics



Dan Tayloe, N7VE

5w Class E 40m Prototype



Why Class E?

Class C final, 2w

40 to 45% efficient, ~ **370 to 410 ma***

Class E final, 2w

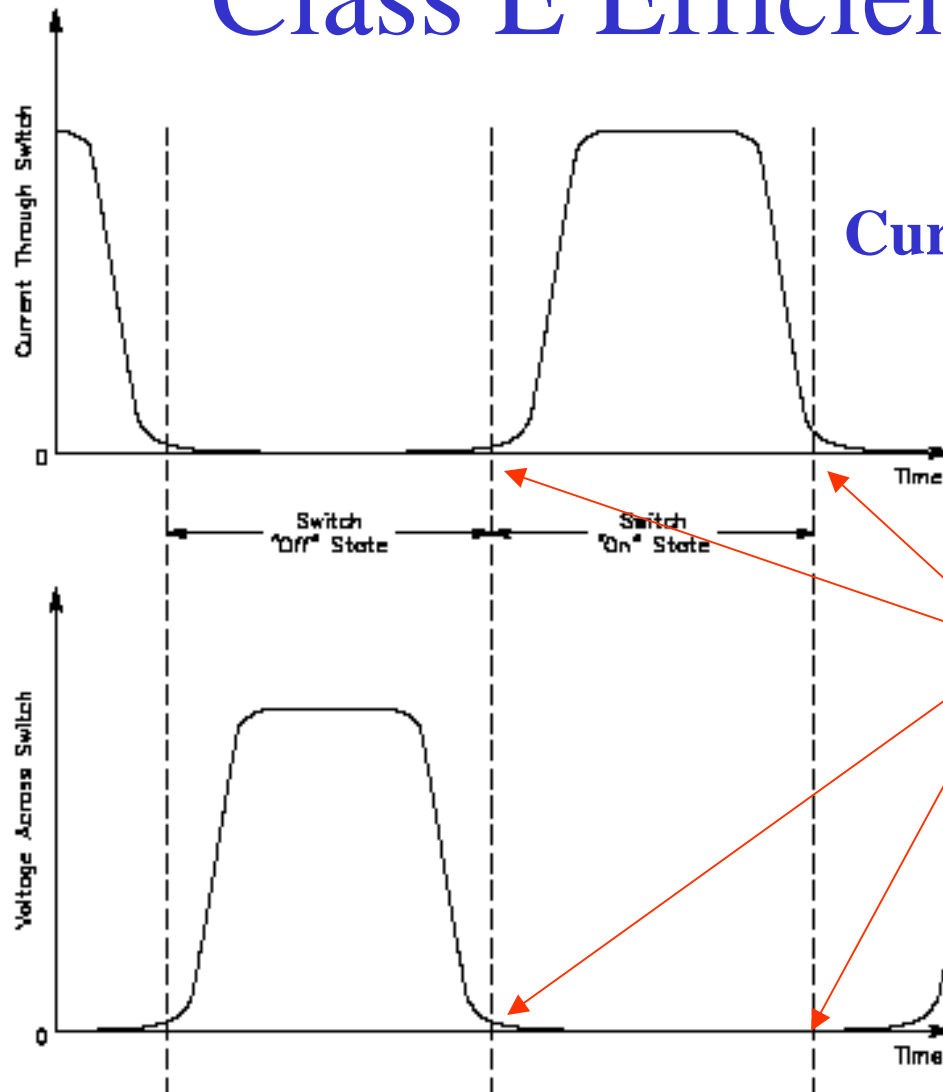
88% efficient, ~ **190 ma***

Almost 50% less TX current required...

Very battery friendly!

** Does not include PA driver. Class E can require very little driver power!*

Class E Efficiency Secret



Current vs. time

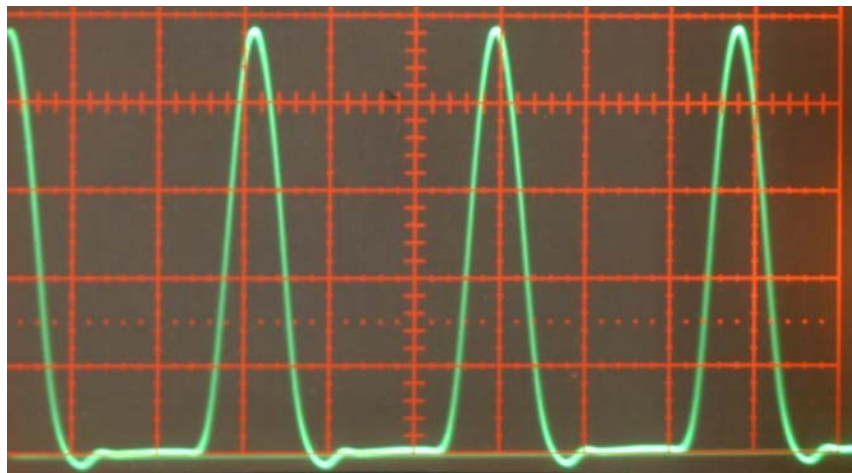
*Switch at low current,
Low voltage points
~Zero power at switch!*

Voltage vs. time

Taken from QEX Jan/Feb 2001

Fig 1—Conceptual “target” waveforms of transistor voltage and current.

Class E Drain Voltage Waveform



Scale 10v/division

~ 48v at peaks for 5 w, ~40v for 2w

For comparison, Class C devices run only 24v peaks

Class E Design Spread Sheet, 7 MHz

QEX Jan/Feb 2001 Class E Design Equations

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O				
1	Class E Output Network Calculator																	
2	QL must be larger than 1.788. Normally, Q<5.																	
3																		
4	User Inputs				User Outputs													
5																		
6	Input Data				Output Data													
7	P (watts)	Vcc-Vo	Fo (Hz)	QL	C1 (pf)	L1 (uh)	L2 (uh)	C2 (pf)	R Load	XC1	XL1	XL2	XC2					
8	2.25	10	7.00E+06	2.92	243	66	1.36	748	20.5	93.8	2900	59.8	30.4					
9																		
10																		
11																		
12																		
13																		
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29																		

Set XL1 above larger than:
2813

L1 FT37-43	L2 T37-2		
AI	Turns	AI	Turns
420	12.5	40	18.4

Note: Need to Subtract Transistor output C from C1

Trans Cout Fix	
Qc	New C1
20	223

Efficiency Estimate - 2x BS170		
Ron (ohm)	tf (nsec)	Efficiency
1	15	87%

High Efficiency
At 7 MHz

Use Q and exact Power to get C1, L2, C2 to standard values

Class E Design Spread Sheet, 14 MHz

QEX Jan/Feb 2001 Class E Design Equations

Class E Output Network Calculator													
QL must be larger than 1.788. Normally, Q<5.													
User Inputs							User Outputs						
Input Data				Output Data									
P (watts)	Vcc-Vo	Fo (Hz)	QL	C1 (pf)	L1 (uh)	L2 (uh)	C2 (pf)	R Load	XC1	XL1	XL2	XC2	
2.25	10	1.40E+07	2.92	121	33	0.68	374	20.5	93.8	2900	59.8	30.4	
										Set XL1 above larger than:			
										2813			
					L1 FT37-43		L2 T37-2						
					Al	Turns	Al	Turns					
					420	8.9	40	13.0					
Note: Need to Subtract Transistor output C from C1													
Trans Cout Fix													
Qc New C1													
20 101													
Efficiency Estimate - 2x BS170													
Ron (ohm) tf (nsec) Efficiency													
1 15 69%													

Reduced Efficiency At 14 MHz

Lower efficiency at 14 MHz – 69% Predicted

Class E Design Spread Sheet

Excel spread sheet equations...

$$C1 \text{ (pf)} = (1e12/(J8*34.2219*D8))*(0.99866 + 0.91424/(E8) - 1.03175/(E8*E8)) + 0.6/(2*2*3.14*3.14*D8*D8*G8/1000000)$$

$$C2 \text{ (pf)} = (1e12/(J8*2*3.14*D8))*(1/(E8-0.104823)) * (1.00121 + 1.01468/(E8 - 1.7879)) - 0.2/(2*2*3.14*3.14*D8*D8*G8/1000000)$$

$$L1 \text{ (uH)} = 1000000*L8/(2*3.14*D8)$$

$$L2 \text{ (uH)} = 1000000*J8*E8/(2*3.14*D8)$$

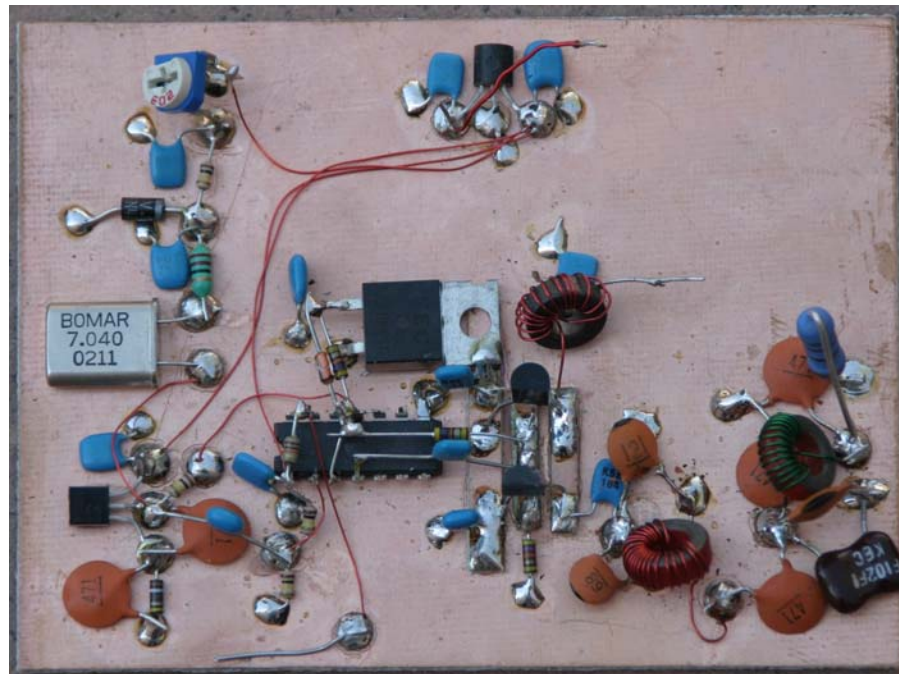
$$Rload = (C8*C8/B8)*0.576801*(1.001245 - 0.451759/E8 - 0.402444/(E8*E8))$$

$$XL1 \geq 30*K8$$

$$\text{Efficiency} = J8/(J8+1.365*K27) - 0.01 - (1 + 0.82/E8)* (1 + 0.82/E8)*4*PI()*PI()*D8*D8*L27*L27*1e-18/12$$

Class E Amplifiers

Part 2: No Tune, Goof Proof Class E Amps



Dan Tayloe, N7VE

Problems with Class E QRP Amps

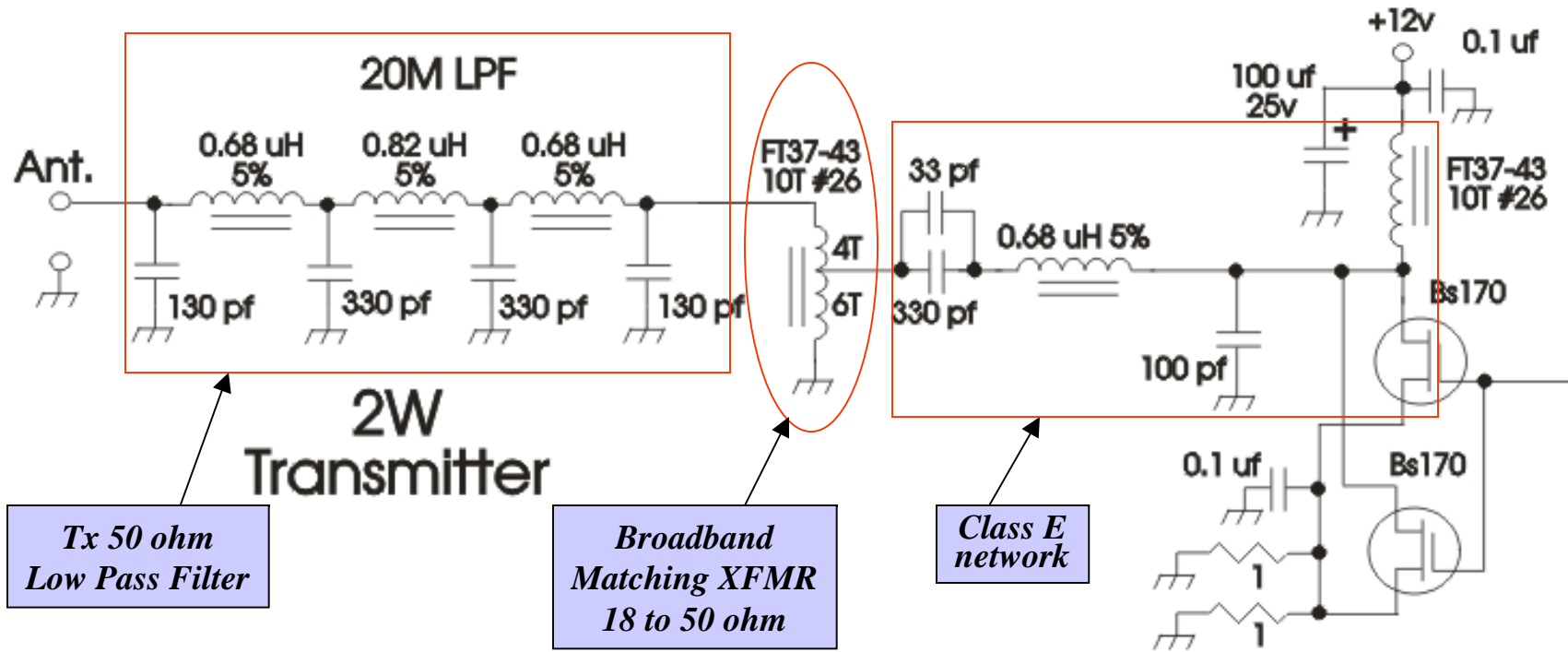
- *“Tuning” required to get good efficiency*
 - Poor “out of the box” power and efficiency
 - Typical to “tweak” output network coils for best power/efficiency
- *Class E finals fail when presented with low impedance loads*
 - Low impedance loads cause PA to draw too much current and burn up
- *Inexpensive QRP Class E final rated to only 60v (2N7000)*
 - Typical PA drain voltage operates in the 40 to 50v range w/ 12v supply
 - Improper antenna mismatch can raise drain voltage, blow the PA
 - *15v supply used with a 12v design could cause problems*
- *Class E Amps can be unstable into poorly matched loads*
 - Tends to “take off”
 - Can lead to device failure

Class E Tuning Problem

- *Class E matching network typically presents a reactive load*
 - I.e., the Class E PA output impedance is *not* purely resistive
 - Reactive characteristic key to Class E efficiency
- *QRP Class E networks need loads in the 10 ohm to 50 ohm (5w to 1w) range*
 - Matching network normally needed to transform to 50 ohm load
 - *1 watt 12v final is a design “sweet spot” – no matching needed*
- *L/C matching networks are typically used to transform driver impedance to 50 ohm load impedance.*
 - This approach does not work well with a reactive drive source!
 - Leads to frequency specific matching network
 - Variations in driver network and matching network elements force the need for “tuning” of the matching networks

No Tune Class E

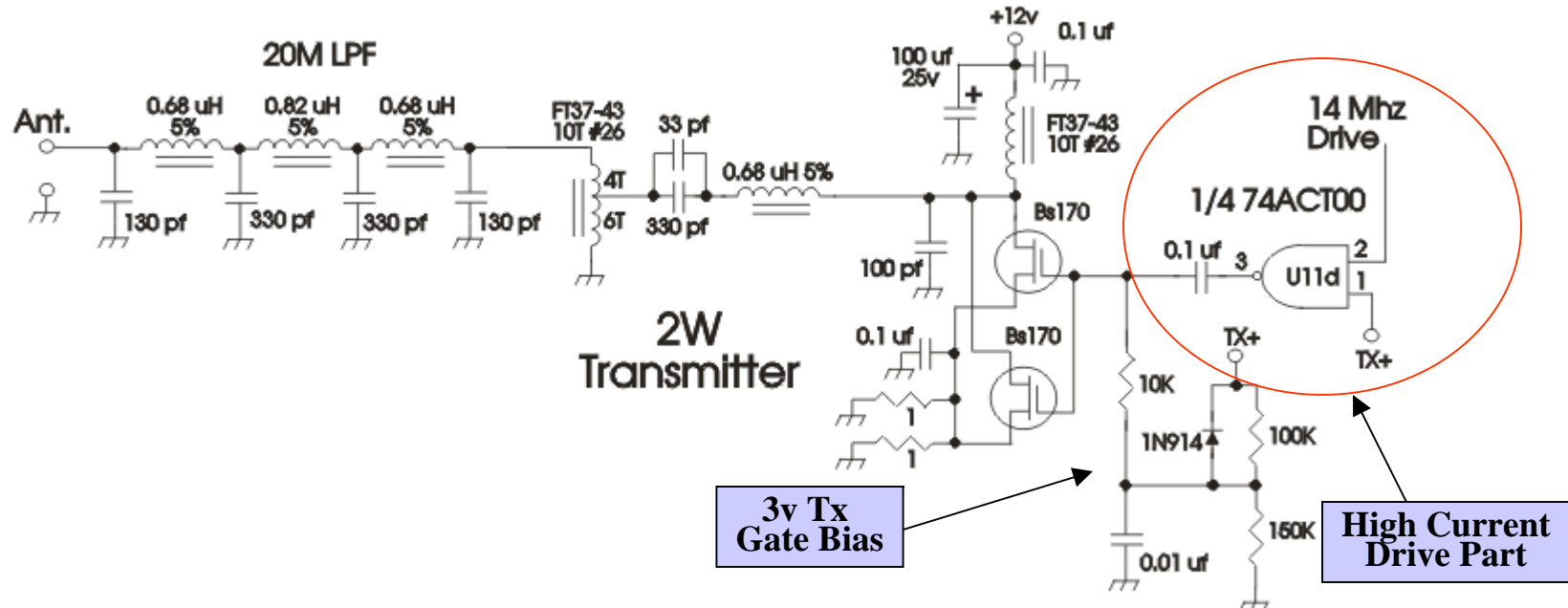
Solution: Use a broadband matching transformer!



- *Broadband Transformer matches 20 ohm PA output to 50 ohm LPF*
- *Transformer converts Class E reactive impedance without being frequency selective*
- *However, efficiency is lower (~60%) as measured on 20 & 30m*

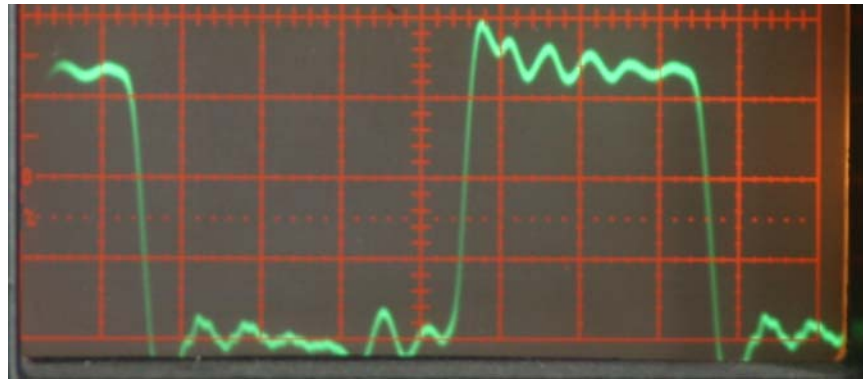
Class E Load Instability

Solution: Use a lower impedance gate driver!



- *AC family has 24 ma of drive vs 8 ma for HC family*
- *Higher current drive = lower drive source impedance*
- *3x lower source impedance reduces tendency to “flight” with mismatched load*
- *PA gate biased on TX to 3v to help MOSFET turn on harder*

Class E Driver – 74ACT00



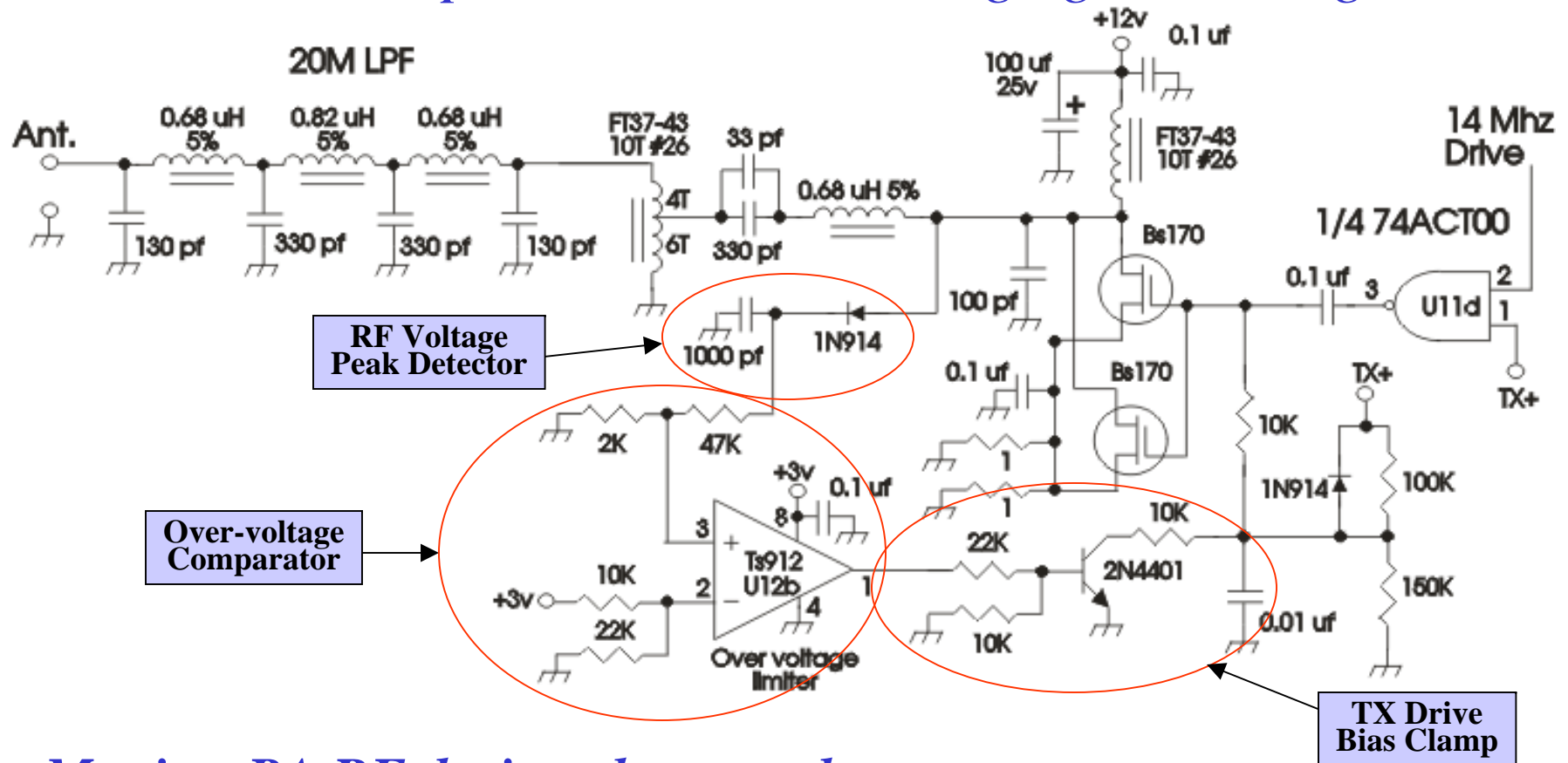
Scale: Vertical 2v/div, Horizontal 20 nsec/div
6 to 8v at peaks

Very fast rise+fall times: ~10 nsec total

*74ACT00 has 24 ma of drive vs. only 8 ma for
the more common 74HCT00 parts*

Class E Voltage Limitations

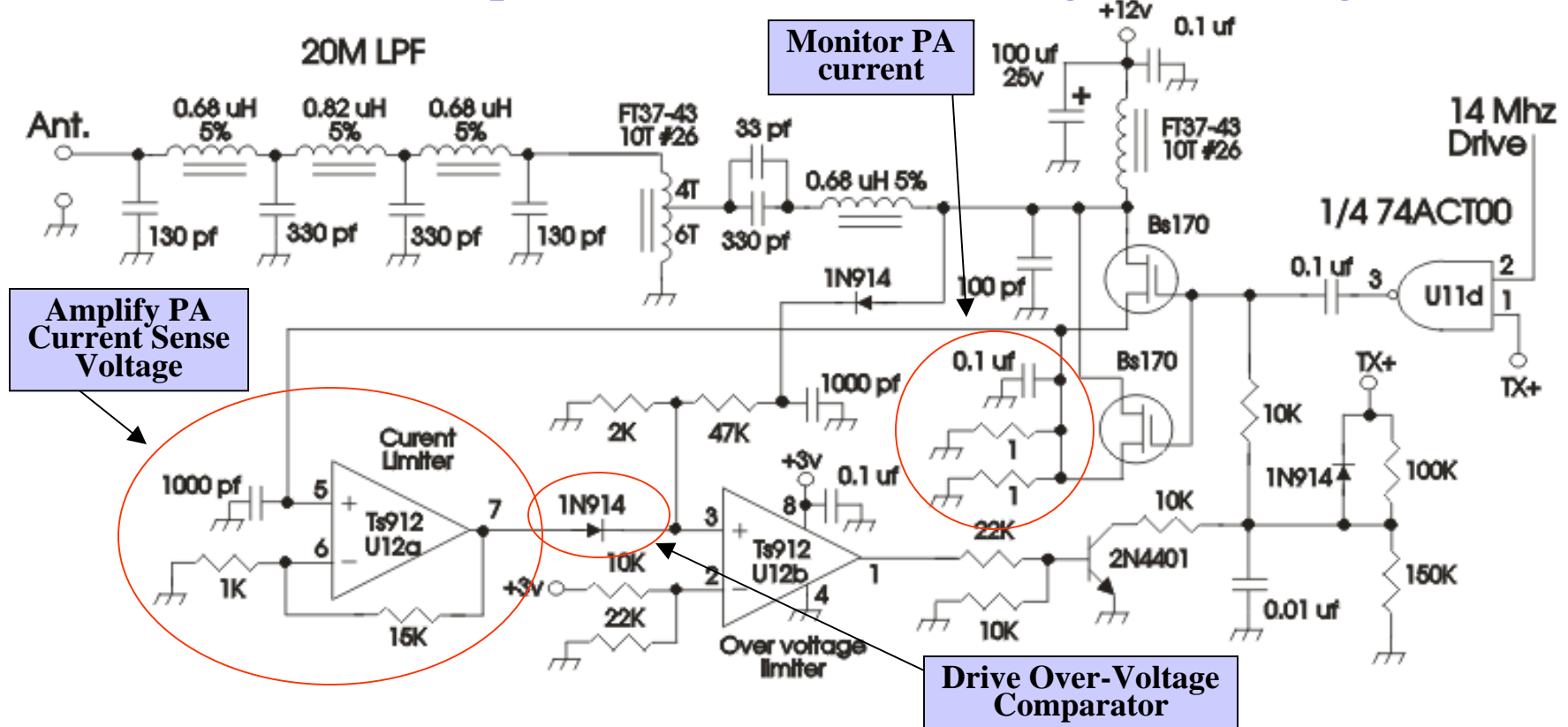
Reduce output when drain voltage gets too high!



- *Monitor PA RF drain voltage peaks*
- *If voltage gets higher than **55v**, comparator triggers bias clamp*
- *Reducing TX gate bias voltage reduces output power to safe limits*

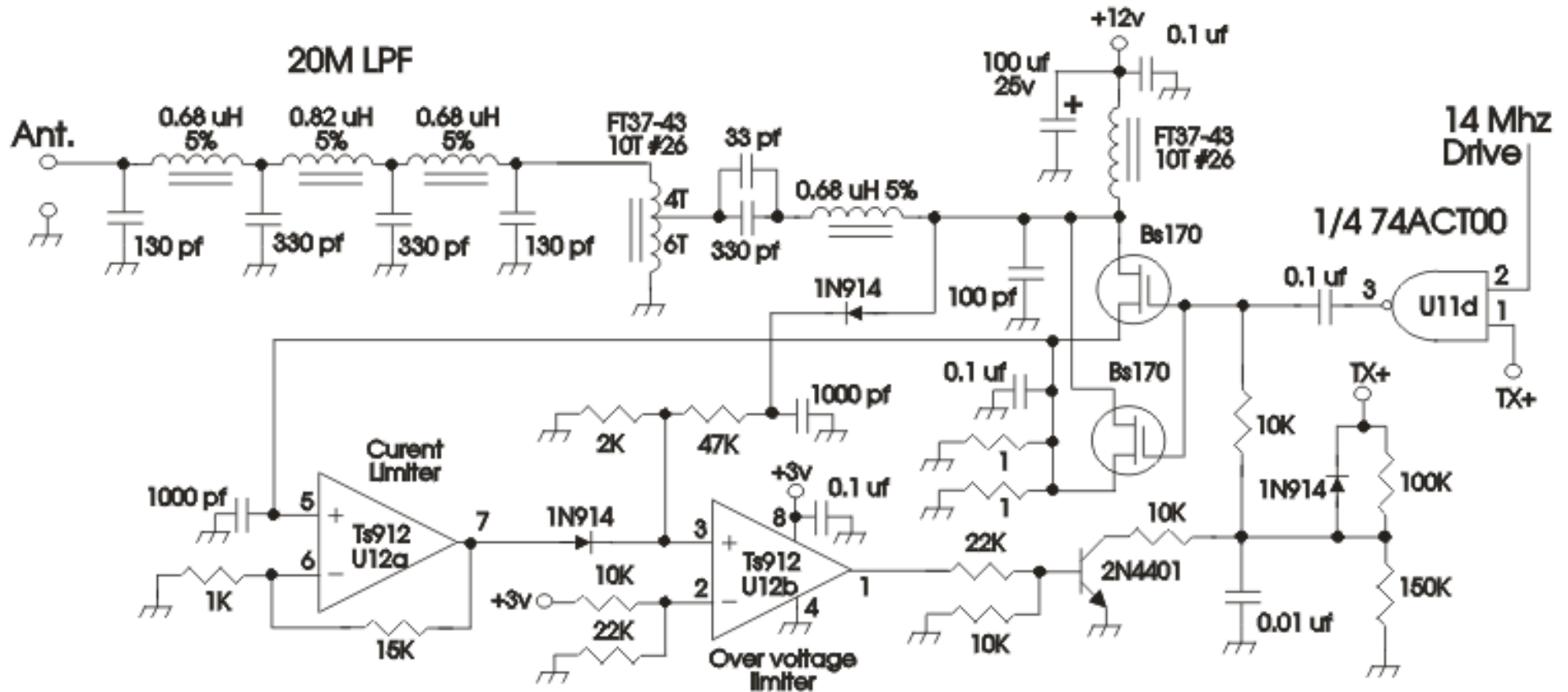
Class E Low Load Limitations

Reduce output when PA current gets too high!



- *Use resistor voltage drop to sense PA current ($\sim 0.175\text{v}$ @ 0.35A)*
- *Amplify sense resistor voltage by 15x ($\sim 2.6\text{v}$ max)*
- *Use amplified voltage (less 0.6v) to trigger over-voltage circuit*
- *Trigger reduces PA gate bias & TX output power, limits PA current*

No Tune, Goof Proof, Class E Tx



- *High impedance over-voltage protection*
- *Low impedance over-current protection*
- *“No Tune” Class E output*

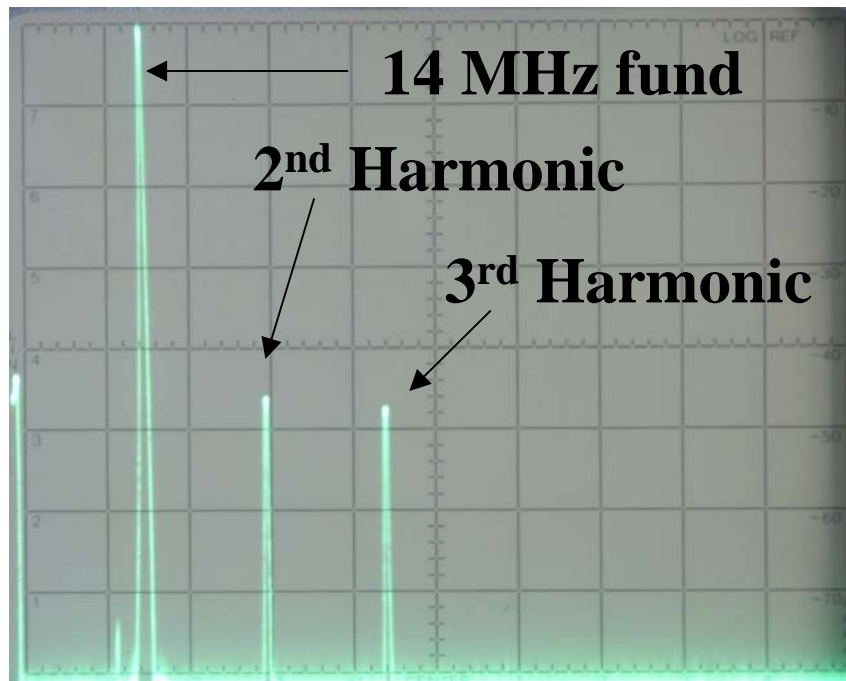
Current Class E Limitations

- Efficiency of common QRP PA devices (2N7000, BS170) drops off at *14 MHz and above*
 - *~80 to 90%* efficiency at 10 MHz and below
 - *~70%* efficiency at 14 MHz
 - *~60 % efficiency using “no tune” approach shown here*
 - R/C freq response: Smaller Driver R = Higher Freq response
 - *Higher PA drive power can be used to get higher freq PA response*
 - *Higher PA drive power hurts overall transmitter power saving*
- Higher frequency devices available, but more expensive
 - *Example: STMicroelectronics PD57006s 900 MHz 5w FET, ~\$12*

Current Class E Limitations, cont

- Class E operates at a *fixed power* set by Class E output network
- Variable power best done by changing supply voltage
- May be able to reduce power from preset maximum by lowering TX gate drive bias, but at reduced TX efficiency.

Transmitter Spectrum



Scale 10 db/division – legal limit 30 db down

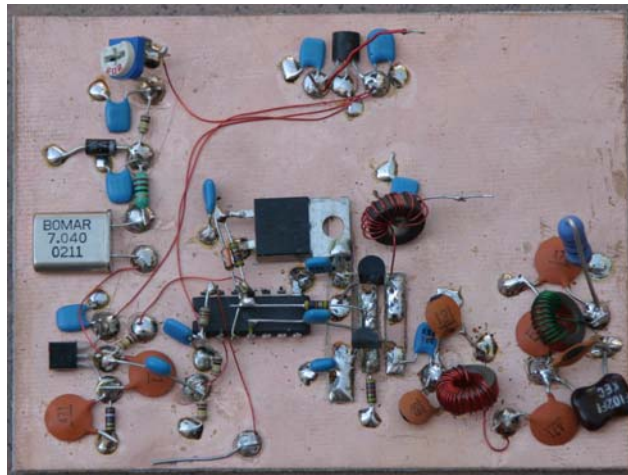
2nd Harmonic *~45 db* down

3rd Harmonic *~47 db* down

All other more than 70 db down

Class E Amplifiers

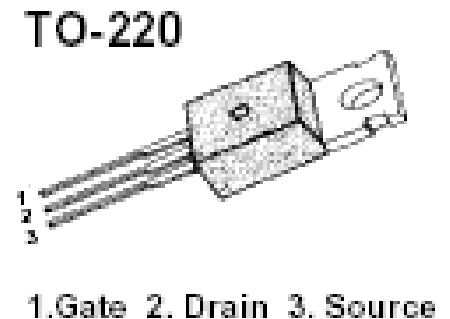
Part 3: Good & Bad QRP Class E Devices Or “Bigger is not Better”



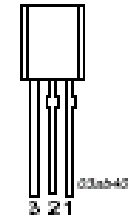
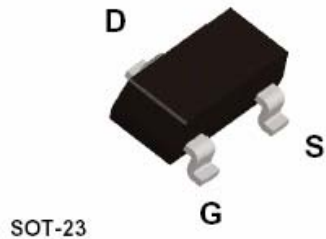
Dan Tayloe, N7VE

Why the IRF510 Makes a Good 5w Class C PA

- IRF510 on/off time 70 nsec, good to 14 MHz
- 40 to 45% efficiency typical using broadband, low pass TX output filters
- **5w** output requires **11.1w** input power
 - **6.1w** of heat produced!
 - **33w IRF510 can take the heat if proper heat sink is used**

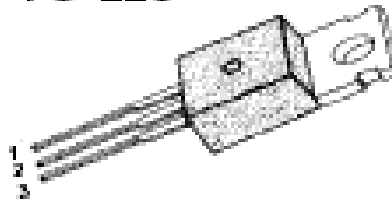


Why the 2N7000 makes a **good** QRP Class E final



and the IRF510 *does not*

TO-220



1. Gate 2. Drain 3. Source

Good FET – 2N7000, 0.3 to 0.6w

Dynamic characteristics						
g_{fs}	forward transconductance	$V_{DS} = 10\text{ V}; I_D = 200\text{ mA};$ Figure 11	100	300	–	mS
C_{iss}	input capacitance	$V_{GS} = 0\text{ V}; V_{DS} = 10\text{ V};$ $f = 1\text{ MHz};$ Figure 12	–	25	40	pF
C_{oss}	output capacitance		–	18	30	pF
C_{rss}	reverse transfer capacitance		–	7.5	10	pF
t_{on}	turn-on time	$V_{DD} = 50\text{ V}; R_D = 250\ \Omega;$	–	3	10	ns
t_{off}	turn-off time	$V_{GS} = 10\text{ V}; R_G = 50\ \Omega;$ $R_{GS} = 50\ \Omega$	–	12	15	ns

Low input C: 25 pf typical – Low input drive drive!

Fast Turn on/off time: 3+12 nsec = 15 nsec

For class E, need On/Off to be 30% of 1/2 RF cycle (QEX 1/01)

- Gives maximum limit of 10 MHz for full efficiency
- Can be used at 14 MHz at reduced efficiency
 - Measured 80-90% at 7 & 10 MHz, 70% at 14 MHz

Difficult FET – IRF510, 33w

C_{iss}	Input Capacitance	--	190	240	pF	$V_{GS}=0V, V_{DS}=25V, f=1MHz$ <i>See Fig 5</i>
C_{oss}	Output Capacitance	--	55	65		
C_{rss}	Reverse Transfer Capacitance	--	21	25		
$t_{d(on)}$	Turn-On Delay Time	--	10	30	ns	$V_{DD}=50V, I_D=5.6A,$ $R_G=24\Omega$ <i>See Fig 13</i> (4)(5)
t_r	Rise Time	--	14	40		
$t_{d(off)}$	Turn-Off Delay Time	--	28	70		
t_f	Fall Time	--	18	50		

Higher input C: 190 pf typical – Higher input drive needed!

- Specs use **24 ohm** source here vs. **50 ohm** source for 2N7000

Slower Turn on/off time: 10+14+28+18 nsec = **70** nsec

For class E, need On/Off to be 30% of $\frac{1}{2}$ RF cycle

- Gives **maximum limit of 2 MHz** for full efficiency
- Can speed up by using a lower impedance drive source.
 - *Slam it on, slam it off!* – more drive power needed.

Double driver power hit: High input C & Slow switching time

Class E Driver Requirements

IRF510 vs. 2N7000

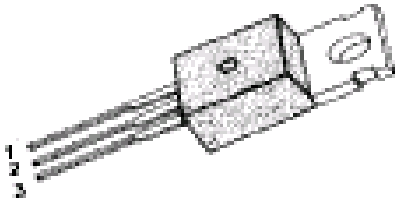
- IRF510, 190 pf input gate C; 2N7000, 25 pf
 - Drive power factor of $7.6x$
- IRF510, 25 ohm source; 2n7000, 50 ohm source
 - Drive power factor of $2x$
- IRF510, 70 nsec turn on/off; 2n7000, 15 nsec
 - Need $4.67x$ lower drive impedance to get same speed
 - IRF510 requires **5 ohm** driver impedance for 15 nsec on/off

Total drive difference: IRF510 needs 71x more drive power than a single 2N7000

- ***~ 0.6w drive for class E IRF511 vs. 17mW for a pair of 2N7000s***

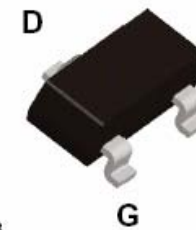
IRF510: Good 100w Class E amp, poor 5w amp!

TO-220

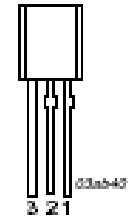


1. Gate 2. Drain 3. Source

Conclusions



SOT-23



SOT54 (TO-92 variant)

- ***Class E saves ~ 50% on TX DC input power to PA***
 - *Low drive power (17 mW vs. 0.6w) saves additional power*
- Class C requires large TO220 PA transistors
- Class E needs only tiny T092/SOT23 300mw/600mw packages
- \$0.14 for a new pair of Class E QRP finals!
- Low wasted TX pwr (***Heat***)
 - *For 5w output, 0.5 to 1w heat (class E) vs. 5 to 6w heat!*
 - Conserves battery life (smaller battery?)
 - Reduces VFO drift

Class E Summary

- *Class E can give up to 88% efficiency*
 - But require tuning to get proper power output
- *Protection circuitry available for Class E finals*
 - Protects against antenna open/short/mismatch problems
- *“No Tune” Class E works, but ~60% efficiently*
- *Bigger is not better for Class E finals*
 - High power MOSFETs (such as the IRF511) require high drive power (*71x!*), reducing overall rig efficiency.